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**Adjusting of Isotope Ratios Measurements by the Method of Least Squares  
on a Programmable Pocket Calculator**

Wyrównywanie mierzonych stosunków izotopowych metodą najmniejszych kwadratów  
za pomocą kieszonkowego kalkulatora programowanego

Исправление измеряемых изотопных отношений методом наименьших квадратов  
с помощью программируемого калькулятора

**INTRODUCTION**

Three or more isotopic elements as strontium and lead are widely utilized in the dating of rocks. Thus a need arises for faster data processing with statistical methods. The usual way of meeting this demand in the case of new instruments is an incorporation of a computer, via an interface and a direct statistical adjustment of the data obtained during mass spectrometric measurements. However, many older instruments still working in scientific laboratories are not equipped with such devices and statistical processing of the data obtained must be performed in a computer centre. The purpose of this paper is to eliminate such inconvenient step by using a simple programmable calculator which can be even communicated with the mass spectrometer employing a home-made interface similar to that described by Hałas and Skorzynski [2].

The Authors have accomplished this goal using inexpensive TI Programmable 59 calculator produced by Texas Instruments. This calculator has up to 100 registers available for data storage or up to 960 for program storage. The memory area can be optionally divided between these two needs. The calculator reads and writes magnetic cards.

**TERMINOLOGY AND METHODS**

Let us consider a mass spectrum of an element for which three peaks are measured. As

an example may serve the mass spectrum of strontium (Fig. 1) in which the isotopic ratio  $^{87}\text{Sr}/^{86}\text{Sr}$  is of geological interest.

However, if the measurements will be limited merely to this ratio, the obtained result can be altered by both systematic and random errors. In order to reduce the systematic error the final value of isotopic ratio is normalized by the following equation [3]:

$$\frac{^{87}\text{Sr}}{^{86}\text{Sr}} = \left[ \frac{(^{87}\text{Sr}/^{86}\text{Sr})_m \ (^{88}\text{Sr}/^{86}\text{Sr})_n}{(^{88}\text{Sr}/^{87}\text{Sr})_m} \right]^{1/2}, \quad (1)$$

where index  $m$  refers to measured ratios and  $n$  to a normalized one (known with a higher accuracy). In order to reduce the random errors, the measured ratios, being utilized in the above equation, should be adjusted by the Least Squares Method. For this reason all major peaks should be measured and three ratios must be calculated.

To unify the notation for strontium and lead isotopes (Fig. 1, 2), the heights of peaks  $^{86}\text{Sr}$ ,  $^{87}\text{Sr}$  and  $^{88}\text{Sr}$  will be denoted as  $x_2$ ,  $x_3$  and  $x_4$ , and their ratios as:

$$\begin{aligned} y_4 &= x_3/x_2 \\ y_5 &= x_4/x_2 \\ y_6 &= x_4/x_3 \end{aligned} \quad (2)$$

These three values are not independent, but are connected by the following rigorous equation:

$$\eta_4 \eta_6 - \eta_5 = 0, \quad (3)$$

where  $\eta$ 's denote the true values of respective  $y$ 's.

Each of the determined ratios will be considered as a sum of true value and of an attached error. A set of the measured values, generally, does not satisfy the rigorous equation. According to the Method of Least Squares, however, the weighted sum of squares of errors can be minimized, thus providing the most reliable estimates of the determined values which satisfy the rigorous equations (see, for instance [1]).

In the formulation of general equations it is convenient to use the ordinary matrix notation. In this notation the determined values, in our example the strontium isotope ratios, will be denoted as one column matrix, i.e. vector:

$$\mathbf{y} = \begin{bmatrix} y_4 \\ y_5 \\ y_6 \end{bmatrix} = \begin{bmatrix} ^{87}\text{Sr}/^{86}\text{Sr} \\ ^{88}\text{Sr}/^{86}\text{Sr} \\ ^{88}\text{Sr}/^{87}\text{Sr} \end{bmatrix}. \quad (4)$$

The variances of  $y$ 's, i.e. squared standard errors, will be represented by diagonal elements of the variance-covariance matrix:

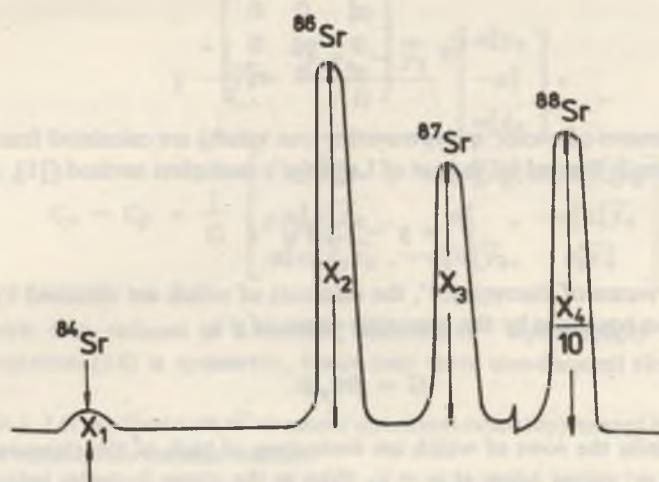


Fig. 1. Mass spectrum of strontium; the height of peaks are proportional to the abundances of the respective isotopes. Three major peaks are measured to reduce statical error of  $^{87}\text{Sr}/^{86}\text{Sr}$  ratio; note that the height of the  $^{88}\text{Sr}$  peak has been reduced by one-tenth

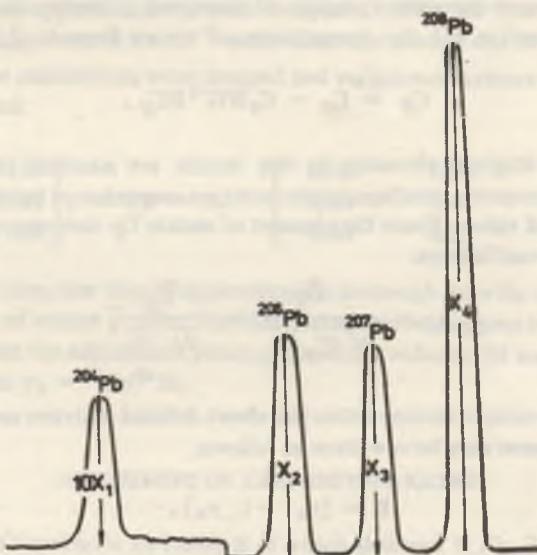


Fig. 2. Mass spectrum of lead, note that the height of the  $^{204}\text{Pb}$  has been enlarged by tenfold

$$C_y = \begin{bmatrix} \sigma_4^2 & 0 & 0 \\ 0 & \sigma_5^2 & 0 \\ 0 & 0 & \sigma_6^2 \end{bmatrix}. \quad (5)$$

The first estimates of vector  $\bar{\eta}$  (representing true values) are calculated from the following general formula derived by the use of Lagrange's multipliers method ([1], chapter 9):

$$\bar{\eta} = \eta - C_y B' G^{-1} c \quad (6)$$

where  $c$  is the 'vector of discrepancy', the elements of which are obtained by replacing  $\eta$ 's in the rigorous equations by the respective values of  $y$ 's,

$$G = BC_y B', \quad (7)$$

and  $B$  is the matrix the rows of which are derivatives of each of the rigorous equations with respect to  $\eta_j$ ; values taken at  $\eta_j = y_j$ . Prim in the above formulas indicates that a given matrix is transposed.

As usual in nonlinear problems the first estimates may not sufficiently satisfy the rigorous equation, therefore iterative procedure should be used: the second approximation of the vector  $\bar{\eta}$  can be calculated again from the above equations by putting  $\bar{\eta}$  instead of the initial vector  $\eta$  in matrix  $B$ , vector  $c$  and equation (6). Further approximations, if necessary, can be calculated in the same way.

Finally, the variance-covariance matrix of improved  $\bar{\eta}$  vector can be calculated by applying to equation (6) the propagation of errors formula ([1], chapter 4-5):

$$C_{\bar{\eta}} = C_y - C_y B' G^{-1} B C_y. \quad (8)$$

Square roots of diagonal elements in this matrix are standard errors of improved values  $\bar{\eta}$ , whereas symmetric nondiagonal elements are covariances between the individual pairs of the improved values. From the element of matrix  $C_{\bar{\eta}}$  one may calculate the estimates of correlation coefficients:

$$\rho_{ij} = \frac{C_{ij}}{\sqrt{C_{ii} C_{jj}}} = \frac{C_{ij}}{\tilde{\sigma}_i \tilde{\sigma}_j}. \quad (9)$$

In the case of strontium isotope ratios the above defined matrices and formulas of the Method of Least Squares may be rewritten as follows:

$$B = (y_6, -1, y_4), \quad (10)$$

$$BC_y = (\sigma_4^2 y_6, -\sigma_5^2, \sigma_6^2 y_4), \quad (11)$$

$$G = \sigma_4^2 y_6^2 + \sigma_5^2 + \sigma_6^2 y_4^2, \quad (12)$$

$$\mathbf{y} - \tilde{\mathbf{y}} = \frac{y_4 y_6 - y_5}{G} \begin{bmatrix} \sigma_4^2 y_6 \\ -\sigma_5^2 \\ \sigma_6^2 y_4 \end{bmatrix}, \quad (13)$$

$$\mathbf{C}_y - \mathbf{C}_{\tilde{y}} = \frac{1}{G} \begin{bmatrix} \sigma_4^2 \tilde{y}_6^2 & -\sigma_4^2 \sigma_5^2 \tilde{y}_6 & \sigma_4^2 \sigma_6^2 \tilde{y}_4 \tilde{y}_6 \\ -\sigma_4^2 \sigma_5^2 \tilde{y}_6 & \sigma_5^4 & -\sigma_5^2 \sigma_6^2 \tilde{y}_4 \\ \sigma_4^2 \sigma_6^2 \tilde{y}_4 \tilde{y}_6 & -\sigma_5^2 \sigma_6^2 \tilde{y}_4 & \sigma_6^4 \tilde{y}_4^2 \end{bmatrix}. \quad (14)$$

Here matrix G is reduced to a number, therefore  $G^{-1}$  equals simply 1/G. Note that matrix in equation (14) is symmetric, hence only three non-diagonal elements must be calculated.

**Example 1.** Let us adjust a set of measured strontium ratios represented by the following vector  $\mathbf{y}$  and variance-covariance matrix:

$$\mathbf{y} = \begin{bmatrix} y_4 \\ y_5 \\ y_6 \end{bmatrix} = \begin{bmatrix} 0.7122 \\ 8.3625 \\ 11.7316 \end{bmatrix}, \quad \mathbf{C}_y = \begin{bmatrix} 0.81 \times 10^{-6} & 0 & 0 \\ 0 & 4.84 \times 10^{-6} & 0 \\ 0 & 0 & 7.84 \times 10^{-6} \end{bmatrix}.$$

The initial 'discrepancy vector' is  $-0.00725$ . Using equations (12), (13) and (14) the first and the second approximations were computed. After the first approximation the 'vector of discrepancy' was  $1.9 \times 10^{-7}$  while after the second one it became as small as  $-2.7 \times 10^{-11}$ , so the calculations were stopped and variance-covariance matrix of improved values was calculated:

$$\tilde{\mathbf{y}} = \begin{bmatrix} 0.7128 \\ 8.3622 \\ 11.7319 \end{bmatrix}, \quad \mathbf{C}_{\tilde{y}} = 10^{-6} \begin{bmatrix} 0.06 & 0.38 & -0.44 \\ 0.38 & 4.65 & 0.22 \\ -0.44 & 0.22 & 7.58 \end{bmatrix}.$$

Actually, in this case, one step of approximation is enough since the differences between the same elements of vector  $\tilde{\mathbf{y}}$ , after the first and the second approximations, are smaller than  $10^{-7}$ . Note that the adjustment process essentially reduces the variance of geochemically important ratio  $y_4 = {}^{87}\text{Sr}/{}^{86}\text{Sr}$ .

#### ADJUSTMENT OF LEAD ISOTOPE RATIOS

In the case of lead spectrum an example of which is shown in Fig. 2, the accurate determination of three isotope ratios, namely  ${}^{206}\text{Pb}/{}^{204}\text{Pb}$ ,  ${}^{207}\text{Pb}/{}^{204}\text{Pb}$  and  ${}^{208}\text{Pb}/{}^{204}\text{Pb}$ , is important in many geo- and cosmochemical studies. These ratios are well known as X, Y and Z values in scientific papers. In our notation they will be represented by  $y_1$ ,  $y_2$  and

$y_3$  values, respectively. Further three ratios which can be determined from four peaks at the mass spectrum, are usually chosen in the following order:

$$y_4 = {}^{207}\text{Pb}/{}^{206}\text{Pb}, \quad y_5 = {}^{208}\text{Pb}/{}^{206}\text{Pb}, \quad y_6 = {}^{208}\text{Pb}/{}^{207}\text{Pb}.$$

We will denote the heights of peaks by  $x_1, x_2, x_3$  and  $x_4$ . Let vector  $\mathbf{y}$  represent six ratios to be determined:

$$\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \\ y_3 \\ y_4 \\ y_5 \\ y_6 \end{bmatrix} = \begin{bmatrix} x_2/x_1 \\ x_3/x_1 \\ x_4/x_1 \\ x_3/x_2 \\ x_4/x_2 \\ x_4/x_3 \end{bmatrix}. \quad (15)$$

From the above matrix equation it follows that these measurements are connected by three independent equations. Further calculations will be based on the following set of rigorous equations:

$$\begin{aligned} \eta_1 \eta_4 - \eta_2 &= 0 \\ \eta_1 \eta_5 - \eta_3 &= 0 \\ \eta_2 \eta_6 - \eta_3 &= 0 \end{aligned} \quad (16)$$

This set provides the design matrix

$$\mathbf{B} = \begin{bmatrix} y_4 & -1 & 0 & y_1 & 0 & 0 \\ y_5 & 0 & -1 & 0 & y_1 & 0 \\ 0 & y_6 & -1 & 0 & 0 & y_2 \end{bmatrix} \quad (17)$$

and the vector of discrepancy<sup>8</sup>

$$\mathbf{c} = \begin{bmatrix} y_1 y_4 - y_2 \\ y_1 y_5 - y_3 \\ y_2 y_6 - y_3 \end{bmatrix}. \quad (18)$$

which can be used in the data adjustment with general formulas (6) and (8). Let us consider a numerical example.

Example 2. For a lead sample the following data were experimentally obtained, represented by the vector

$$\mathbf{y} = \begin{bmatrix} 16.07 \\ 15.49 \\ 36.78 \\ 0.9651 \\ 2.2891 \\ 2.3726 \end{bmatrix}$$

and variance-covariance matrix

$$C_y = 10^{-4} \begin{bmatrix} 624 & 0 & 0 & 0 & 0 & 0 \\ 0 & 556 & 0 & 0 & 0 & 0 \\ 0 & 0 & 3472 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.0441 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0.2025 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0.3136 \end{bmatrix}.$$

The initial 'discrepancy vector' is

$$c = \begin{bmatrix} 0.0192 \\ 0.0058 \\ -0.0284 \end{bmatrix}.$$

while after the first step of iterative process (equation (6)) its elements are as small as about  $10^{-7}$ . After the second step they are comparable with machine error  $\approx 10^{-11}$ . Calculations are, therefore, stopped at the second step of approximation, and the improved values and their variance-covariance matrix are obtained:

$$\tilde{y} = \begin{bmatrix} 16.0624 \\ 15.5002 \\ 36.7715 \\ 0.9650 \\ 2.2893 \\ 2.3723 \end{bmatrix}, \quad C_{\tilde{y}} = 10^{-4} \begin{bmatrix} 211 & 200 & 476 & -0.23 & -0.49 & 0.06 \\ 200 & 197 & 458 & 0.24 & -0.02 & -0.62 \\ 476 & 458 & 1109 & -0.08 & 1.23 & 1.47 \\ -0.23 & 0.24 & -0.08 & 0.029 & 0.028 & -0.042 \\ -0.49 & -0.02 & 1.23 & 0.028 & 0.146 & 0.082 \\ 0.06 & -0.62 & 1.47 & -0.042 & 0.082 & 0.189 \end{bmatrix}.$$

This example illustrates that estimates of covariances between the improved ratios  $\tilde{y}_4$ ,  $\tilde{y}_5$ ,  $\tilde{y}_6$  and the others are very small. In contrast to these values, the ratios  $\tilde{y}_1$ ,  $\tilde{y}_2$ ,  $\tilde{y}_3$  are strongly correlated with correlation coefficients approaching the limit value  $\rho = 1$ . Such a behaviour of the elements of variance-covariance matrix and the strong convergence of iterative process indicate that our problem is nearly linear. Actually, as the height of the minor peak is by one order smaller than the rest, its small variation produces large and strongly correlated variations in  $\tilde{y}_1$ ,  $\tilde{y}_2$  and  $\tilde{y}_3$  ratios. Moreover, these three ratios show percentage errors by one order higher than three others. Hence  $\eta_4$ ,  $\eta_5$  and  $\eta_6$  in the set of rigorous equations (16) may be considered as nearly constant.

One may conclude from this discussion that the problem of the adjustment of lead isotope ratios can be divided into two smaller problems: adjustment of  $y_4$ ,  $y_5$ ,  $y_6$  and, then,  $y_1$ ,  $y_2$ ,  $y_3$  ratios. The first problem is identical with that demonstrated above for strontium isotopes, whereas the second problem may be solved in the same way. However, it includes two independent rigorous equations and three measurements to be adjusted. Hence, the method of elements ([1], chapter 9-3) is more convenient than the method of Lagrange multipliers used above.

Putting the adjusted values  $\tilde{y}_4$ ,  $\tilde{y}_5$ ,  $\tilde{y}_6$  into equations (16), one may obtain three

linear equations, but only two linearly independent. Let us choose the following set for further calculations:

$$\begin{aligned}\eta_1 \tilde{y}_4 - \eta_2 &= 0 \\ \eta_1 \tilde{y}_5 - \eta_3 &= 0\end{aligned}\quad (19)$$

Taking  $\eta_1$  as the element, from equation (19) we obtain

$$\eta = \begin{bmatrix} \eta_1 \\ \eta_2 \\ \eta_3 \end{bmatrix} = \begin{bmatrix} 1 \\ \tilde{y}_4 \\ \tilde{y}_5 \end{bmatrix} \quad \eta_1 = F\eta_1. \quad (20)$$

To solve our adjusting problem one column matrix  $F$ , thus obtained, must be put in the following expressions:

$$C_{\tilde{y}} = \frac{FF'}{H} = \frac{1}{H} \begin{bmatrix} 1 & \tilde{y}_4 & \tilde{y}_5 \\ \tilde{y}_4 & \tilde{y}_4^2 & \tilde{y}_4 \tilde{y}_5 \\ \tilde{y}_5 & \tilde{y}_4 \tilde{y}_5 & \tilde{y}_5^2 \end{bmatrix}, \quad (21)$$

where

$$H = F C_y^{-1} F = \frac{1}{\sigma_1^2} + \frac{\tilde{y}_4^2}{\sigma_2^2} + \frac{\tilde{y}_5^2}{\sigma_3^2}, \quad (22)$$

and

$$\tilde{y} = C_y C_y^{-1} y = C_{\tilde{y}} \begin{bmatrix} y_1/\sigma_1^2 \\ y_2/\sigma_2^2 \\ y_3/\sigma_3^2 \end{bmatrix}. \quad (23)$$

Note that all correlation coefficients followed from the expression's (21) equal unity, as expected.

**Example 3.** In order to compare the results obtained in this very simplified way with those obtained by the method demonstrated above, let us consider again the same set of initial values  $y$  and  $C_y$  as in Example 2. Our simplified approach provides the following first estimates:

$$\tilde{y} = \begin{bmatrix} 16.0624 \\ 15.5002 \\ 36.7715 \\ 0.9650 \\ 2.2893 \\ 2.3723 \end{bmatrix}, \quad C_{\tilde{y}} = 10^{-4} \begin{bmatrix} 209 & 202 & 478 & 0 & 0 & 0 \\ 202 & 195 & 461 & 0 & 0 & 0 \\ 478 & 461 & 1095 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.029 & 0.029 & -0.043 \\ 0 & 0 & 0 & 0.029 & 0.147 & 0.083 \\ 0 & 0 & 0 & -0.043 & 0.083 & 0.190 \end{bmatrix}.$$

This example clearly shows that in the case of lead isotopes, and also in other cases when one peak is small in comparison with the other to be measured, both methods provide nearly identical adjusted ratios. Also the standard errors and correlation coefficients, derived from simplified  $C_{\bar{y}}$ , are close to those derived from a strict variance-covariance matrix. Even those correlation coefficients which correspond to covariances are estimated here as zero. Therefore, a calculator program will be presented for the simplified procedure only. The program for the strict method on TI Programmable 59 calculator is available from the authors.

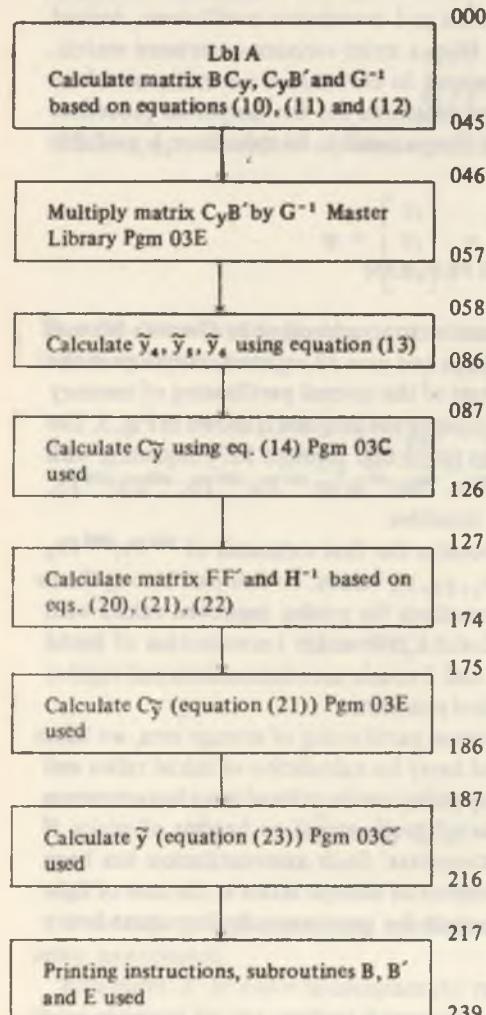
#### THE CALCULATOR PROGRAM

The program listed in the Appendix has been written according to Owner's Manual for TI Programmable 58/59. It consists of 316 steps and uses 33 registers, therefore it can be written on one magnetic card without the reset of the normal partitioning of memory storage area in TI Programmable 59. The flow diagram of the program is shown in Fig. 3. The program consists of two basic parts. The first part (steps 000 through 127) beginning with label A enables the adjusting of  $^{87}\text{Sr}/^{86}\text{Sr}$ ,  $^{88}\text{Sr}/^{86}\text{Sr}$ ,  $^{88}\text{Sr}/^{87}\text{Sr}$  or  $^{207}\text{Pb}/^{206}\text{Pb}$ ,  $^{208}\text{Pb}/^{206}\text{Pb}$ ,  $^{208}\text{Pb}/^{207}\text{Pb}$  ratios, i.e.  $y_4$ ,  $y_5$ ,  $y_6$  in our unified notation.

The second part (steps 128 through 240) provides the first estimates of  $^{206}\text{Pb}/^{204}\text{Pb}$ ,  $^{207}\text{Pb}/^{204}\text{Pb}$ ,  $^{208}\text{Pb}/^{204}\text{Pb}$  ratios noted here as  $y_1$ ,  $y_2$ ,  $y_3$  values. To this part belong three subroutines (labels B, B' and E) including instructions for printing improved values with their standard errors. Subroutine C is designed for a convenient introduction of initial data: ratios and their standard errors. Tables 1 and 2 contain user instructions and register contents. Figure 4 shows two examples of standard printouts.

As numerous free steps are available at the normal partitioning of storage area, we have extended our program to a subroutine (not listed here) for calculation of initial ratios and errors directly from the heights of peaks. This capability can be utilized in an instantaneous adjustment of readouts of digital voltmeter, being proportional to heights of peaks, if the calculator is interfaced with a mass spectrometer. Such automatization has been accomplished in our laboratory for the measurements of isotope ratios in the case of light elements and we are going to extend this technique for geochemically important heavy elements.

## MAIN PROGRAM



## SUBROUTINES

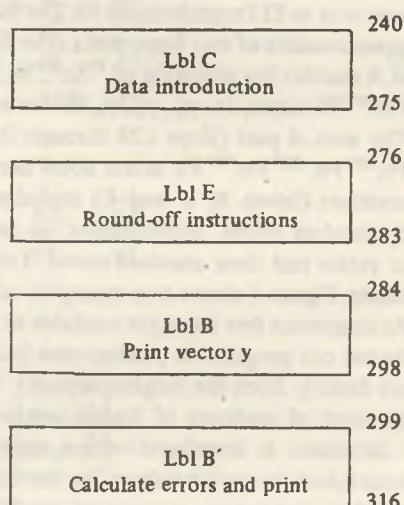


Fig. 3. The flow diagram of the program for adjusting strontium and lead isotope ratios

Tab. 1. User Instructions

| Step | Procedure                                    | Enter                                                                            | Press                                  | Display                                                                                      |
|------|----------------------------------------------|----------------------------------------------------------------------------------|----------------------------------------|----------------------------------------------------------------------------------------------|
| 1    | Initialize                                   |                                                                                  | C                                      | 28                                                                                           |
| 2    | Enter elements of vector $y$                 | $y_1$<br>$y_2$<br>$y_3$<br>$y_4$<br>$y_5$<br>$y_6$                               | R/S<br>R/S<br>R/S<br>R/S<br>R/S<br>R/S | $y_1$<br>$y_2$<br>$y_3$<br>$y_4$<br>$y_5$<br>6                                               |
| 3    | Enter standard errors                        | $\sigma_1$<br>$\sigma_2$<br>$\sigma_3$<br>$\sigma_4$<br>$\sigma_5$<br>$\sigma_6$ | R/S<br>R/S<br>R/S<br>R/S<br>R/S<br>R/S | $\sigma_1^2$<br>$\sigma_2^2$<br>$\sigma_3^2$<br>$\sigma_4^2$<br>$\sigma_5^2$<br>$\sigma_6^2$ |
| 4    | Perform the adjustment of the entered values | A                                                                                | see note 1                             |                                                                                              |

NOTES: 1. Subroutine A provides standard printout, shown in Fig. 4, with 4 decimal places. One may reset this number occupying step 279 of the program.

2. For strontium isotopes perform all above steps with any number as  $y_1, y_2, y_3$  and  $\sigma_1, \sigma_2, \sigma_3$  values.

3. Elements of variance-covariance matrix may be recalled after computations from appropriate registers, see Tab. 2.

Tab. 2. Register Contents

|          |                               |
|----------|-------------------------------|
| $R_{00}$ | $R_{20}$                      |
| $R_{01}$ | $R_{21}$                      |
| $R_{02}$ | $R_{22}$                      |
| $R_{03}$ | $R_{23}$                      |
| $R_{04}$ | $R_{24}$                      |
| $R_{05}$ | $R_{25}$                      |
| $R_{06}$ | $R_{26}$                      |
| $R_{07}$ | $R_{27}$                      |
| $R_{08}$ | $R_{28} y_1$                  |
| $R_{09}$ | $R_{29} y_2$                  |
| $R_{10}$ | $R_{30} y_3$                  |
| $R_{11}$ | $R_{31} y_4, \bar{y}_4$       |
| $R_{12}$ | $R_{32} y_5, \bar{y}_5$       |
| $R_{13}$ | $R_{33} y_6, \bar{y}_6$       |
| $R_{14}$ | $R_{34} c_{11}$               |
| $R_{15}$ | $R_{35} c_{22}$               |
| $R_{16}$ | $R_{36} c_{33}$               |
| $R_{17}$ | $R_{37} c_{44}, \bar{c}_{44}$ |
| $R_{18}$ | $R_{38} c_{55}, \bar{c}_{55}$ |
| $R_{19}$ | $R_{39} c_{66}, \bar{c}_{66}$ |

NOTES: 1. A fraction of memory registers are used twice: the first symbols represent number stored when the first part of the program is running while the second symbols represent numbers which can be recalled after run of the second part.

2. Symbols  $\tilde{c}_{ij}$  were used for the elements of variance-covariance matrix of improved values.

|            |                    |          |                    |
|------------|--------------------|----------|--------------------|
| 28. 0000   |                    | 16. 0700 | $y_1$              |
| 28. 0000   |                    | 15. 4900 | $y_2$              |
| 28. 0000   |                    | 36. 7800 | $y_3$              |
| 0. 7122    | $y_4$              | 0. 9651  | $y_4$              |
| 8. 3625    | $y_5$              | 2. 2891  | $y_5$              |
| 11. 7316   | $y_6$              | 2. 3726  | $y_6$              |
| 6. 0000    |                    | 0. 2498  | $\sigma_1$         |
| 36. 0000   |                    | 0. 2358  | $\sigma_2$         |
| 1296. 0000 |                    | 0. 5892  | $\sigma_3$         |
| 0. 0009    | $\sigma_4$         | 0. 0021  | $\sigma_4$         |
| 0. 0022    | $\sigma_5$         | 0. 0045  | $\sigma_5$         |
| 0. 0028    | $\sigma_6$         | 0. 0056  | $\sigma_6$         |
| 28. 1204   |                    | 16. 0624 | $\tilde{y}_1$      |
| 20. 0435   |                    | 15. 5002 | $\tilde{y}_2$      |
| 235. 1487  |                    | 36. 7715 | $\tilde{y}_3$      |
| 0. 7128    | $\tilde{y}_4$      | 0. 9650  | $\tilde{y}_4$      |
| 8. 3622    | $\tilde{y}_5$      | 2. 2893  | $\tilde{y}_5$      |
| 11. 7319   | $\tilde{y}_6$      | 2. 3723  | $\tilde{y}_6$      |
| 5. 9537    |                    | 0. 1445  | $\tilde{\sigma}_1$ |
| 4. 2436    |                    | 0. 1395  | $\tilde{\sigma}_2$ |
| 49. 7861   |                    | 0. 3309  | $\tilde{\sigma}_3$ |
| 0. 0002    | $\tilde{\sigma}_4$ | 0. 0017  | $\tilde{\sigma}_4$ |
| 0. 0022    | $\tilde{\sigma}_5$ | 0. 0038  | $\tilde{\sigma}_5$ |
| 0. 0028    | $\tilde{\sigma}_6$ | 0. 0044  | $\tilde{\sigma}_6$ |

Fig. 4. Standard format of the printed results; the time of calculation is about 1 min

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2. Hałas S., Skorzyński Z.: J. Phys. E.: Sci. Instrum. 13, 346-349 (1980).
3. Seibt W., Rainer L., Heinz E.: Z. Naturforschg. 18a, 1288-1295 (1963).

## APPENDIX

## PROGRAM LISTING

|            |            |                       |                       |            |                       |
|------------|------------|-----------------------|-----------------------|------------|-----------------------|
| 000 76 LBL | 049 01 1   | 098 37 37             | 147 85 +              | 196 43 RCL | 245 02 2              |
| 001 11 A   | 050 42 STO | 099 43 RCL            | 148 43 RCL            | 197 35 35  | 246 08 8              |
| 002 43 RCL | 051 04 04  | 100 17 17             | 149 36 36             | 198 35 1/X | 247 42 STO            |
| 003 37 37  | 052 00 0   | 101 42 STO            | 150 35 1/X            | 199 65 x   | 248 06 06             |
| 004 65 x   | 053 42 STO | 102 15 15             | 151 65 x              | 200 43 RCL | 249 91 R/S            |
| 005 43 RCL | 054 06 06  | 103 36 PGM            | 152 43 RCL            | 201 29 29  | 250 72 ST*            |
| 006 33 33  | 055 36 PGM | 104 03 03             | 153 32 32             | 202 95 =   | 251 06 06             |
| 007 95 =   | 056 03 03  | 105 18 C'             | 154 42 STO            | 203 42 STO | 252 15 E              |
| 008 42 STO | 057 15 E   | 106 43 RCL            | 155 10 10             | 204 22 22  | 253 69 OP             |
| 009 08 08  | 058 43 RCL | 107 12 12             | 156 42 STO            | 205 43 RCL | 254 26 26             |
| 010 42 STO | 059 31 31  | 108 22 INV            | 157 14 14             | 206 36 36  | 255 97 DSZ            |
| 011 16 16  | 060 65 x   | 109 44 SUM            | 158 33 X <sup>2</sup> | 207 53 1/X | 256 07 07             |
| 012 65 x   | 061 43 RCL | 110 38 38             | 159 42 STO            | 208 65 x   | 257 02 02             |
| 013 43 RCL | 062 33 33  | 111 43 RCL            | 160 16 16             | 209 43 RCL | 258 49 49             |
| 014 33 33  | 063 75 -   | 112 11 11             | 161 95 =              | 210 30 30  | 259 06 6              |
| 015 75 -   | 064 43 RCL | 113 42 STO            | 162 35 1/X            | 211 95 =   | 260 42 STO            |
| 016 43 RCL | 065 32 32  | 114 19 19             | 163 42 STO            | 212 42 STO | 261 07 07             |
| 017 38 38  | 066 95 =   | 115 43 RCL            | 164 05 05             | 213 23 23  | 262 98 ADV            |
| 018 94 +/- | 067 42 STO | 116 18 18             | 165 43 RCL            | 214 36 PGM | 263 91 R/S            |
| 019 42 STO | 068 15 15  | 117 42 STO            | 166 31 31             | 215 03 03  | 264 15 E              |
| 020 09 09  | 069 36 PGM | 118 15 15             | 167 65 x              | 216 18 C'  | 265 33 X <sup>2</sup> |
| 021 42 STO | 070 03 03  | 119 36 PGM            | 168 43 RCL            | 217 01 1   | 266 72 ST*            |
| 022 17 17  | 071 18 C'  | 120 03 03             | 169 32 32             | 218 07 7   | 267 06 06             |
| 023 95 =   | 072 43 RCL | 121 18 C'             | 170 95 =              | 219 42 STO | 268 69 OP             |
| 024 42 STO | 073 11 11  | 122 43 RCL            | 171 42 STO            | 220 06 06  | 269 26 26             |
| 025 05 05  | 074 22 INV | 123 13 13             | 172 15 15             | 221 12 B   | 270 97 DSZ            |
| 026 43 RCL | 075 44 SUM | 124 22 INV            | 173 42 STO            | 222 03 3   | 271 07 07             |
| 027 39 39  | 076 31 31  | 125 44 SUM            | 174 13 13             | 223 01 1   | 272 02 02             |
| 028 65 x   | 077 43 RCL | 126 39 39             | 175 03 3              | 224 42 STO | 273 63 63             |
| 029 43 RCL | 078 12 12  | 127 01 1              | 176 42 STO            | 225 06 06  | 274 98 ADV            |
| 030 31 31  | 079 22 INV | 128 42 STO            | 177 04 04             | 226 12 B   | 275 92 RTN            |
| 031 95 =   | 080 44 SUM | 129 08 08             | 178 04 4              | 227 98 ADV | 276 76 LBL            |
| 032 42 STO | 081 32 32  | 130 43 RCL            | 179 42 STO            | 228 08 8   | 277 15 E              |
| 033 10 10  | 082 43 RCL | 131 34 34             | 180 25 25             | 229 42 STO | 278 58 FIX            |
| 034 42 STO | 083 13 13  | 132 35 1/X            | 181 00 0              | 230 06 06  | 279 04 04             |
| 035 18 18  | 084 22 INV | 133 85 +              | 182 42 STO            | 231 17 B'  | 280 99 PRT            |
| 036 65 x   | 085 44 SUM | 134 43 RCL            | 183 06 06             | 232 03 3   | 281 22 INV            |
| 037 43 RCL | 086 33 33  | 135 35 35             | 184 36 PGM            | 233 07 7   | 282 58 FIX            |
| 038 31 31  | 087 43 RCL | 136 35 1/X            | 185 03 03             | 234 42 STO | 283 92 RTN            |
| 039 85 +   | 088 16 16  | 137 65 x              | 186 15 E              | 235 06 06  | 284 76 LBL            |
| 040 43 RCL | 089 42 STO | 138 43 RCL            | 187 43 RCL            | 236 01 1   | 285 12 B              |
| 041 05 05  | 090 15 15  | 139 31 31             | 188 34 34             | 237 42 STO | 286 03 3              |
| 042 95 =   | 091 36 PGM | 140 42 STO            | 189 35 1/X            | 238 25 25  | 287 42 STO            |
| 043 35 1/X | 092 03 03  | 141 09 09             | 190 65 x              | 239 17 B'  | 288 07 07             |
| 044 42 STO | 093 18 C'  | 142 42 STO            | 191 43 RCL            | 240 76 LBL | 289 73 RC*            |
| 045 05 05  | 094 43 RCL | 143 11 11             | 192 28 28             | 241 13 C   | 290 06 06             |
| 046 03 3   | 095 11 11  | 144 33 X <sup>2</sup> | 193 95 =              | 242 06 6   | 291 15 E              |
| 047 42 STO | 096 22 INV | 145 42 STO            | 194 42 STO            | 243 42 STO | 292 69 OP             |
| 048 03 03  | 097 44 SUM | 146 12 12             | 195 21 21             | 244 07 07  | 293 26 26             |

|     |    |     |     |    |     |     |    |     |     |    |     |     |    |     |
|-----|----|-----|-----|----|-----|-----|----|-----|-----|----|-----|-----|----|-----|
| 294 | 97 | DSZ | 299 | 76 | LBL | 304 | 73 | RC* | 309 | 25 | 25  | 314 | 03 | 03  |
| 295 | 07 | 07  | 300 | 17 | B'  | 305 | 06 | 06  | 310 | 44 | SUM | 315 | 04 | 04  |
| 296 | 02 | 02  | 301 | 03 | 3   | 306 | 34 | ГХ  | 311 | 06 | 06  | 316 | 92 | RTN |
| 297 | 89 | 89  | 302 | 42 | STO | 307 | 15 | E   | 312 | 97 | DSZ |     |    |     |
| 298 | 92 | RTN | 303 | 07 | 07  | 308 | 43 | RCL | 313 | 07 | 07  |     |    |     |

### STRESZCZENIE

Praca zawiera prosty i praktyczny algorytm pozwalający poprawiać stosunki izotopowe dla pierwiastków złożonych z kilku (3–5) izotopów oraz umożliwiający znaczną redukcję błędów losowych obliczanych w ten sposób stosunków.

Algorytm wykorzystuje metodę najmniejszych kwadratów i ma charakter iteracyjny. W przedstawionych przykładach wystarczyły dwa kroki iteracyjne do tego, by różnice między kolejnymi przybliżeniami poprawionych elementów stały się porównywalne z błędem maszynowym (ok.  $10^{-11}$ ). Algorytm został zrealizowany na programowanym kalkulatorze kieszonkowym TI Programmable 59. Opracowany program jest szczególnie użyteczny przy poprawianiu stosunków izotopowych strontu i ołówku.

Dodatki zawierają sieć działań programu, przykładowe tabulogramy wyników oraz wydruk programu.

### РЕЗЮМЕ

В работе излагается простой алгоритм, который позволяет значительно поправлять экспериментальные данные по изотопным отношениям элементов составленных на 3–5 изотопов. В алгоритме, который имеет итерационный характер, используется метод наименьших квадратов. В представленных вычислениях достигается разница между последовательными приближениями поправленных отношений порядка  $10^{-11}$  (машиинной ошибки) в двух итерационных шагах.

Алгоритм реализован на программированном калькуляторе ТИ-59. Разработанная программа особенно полезна для поправления изотопных отношений стронта и свинца. В приложениях представлены: диаграмма действий программы и полная форма программы.

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